



EDDY-TOPOGRAPHY INTERACTIONS AND THE FATE OF THE PERSIAN GULF OUTFLOW

SYNBIOS workshop

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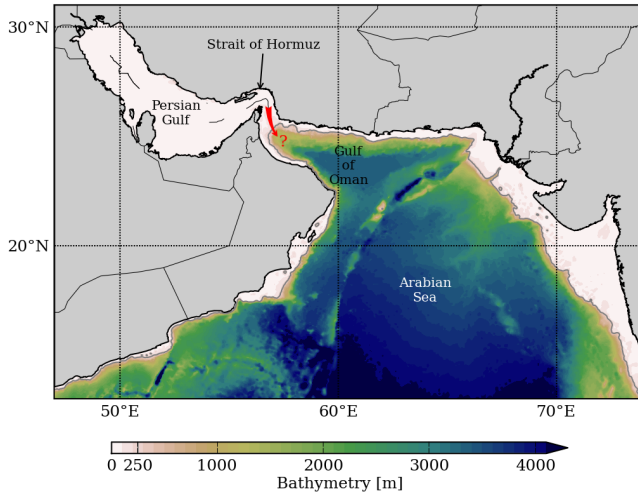
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OUTLINE

1. Context & Issues
2. Phenomenology - Realistic Simulation
3. Processes - Idealized Simulation
4. Turbulent Diffusion
5. Conclusions

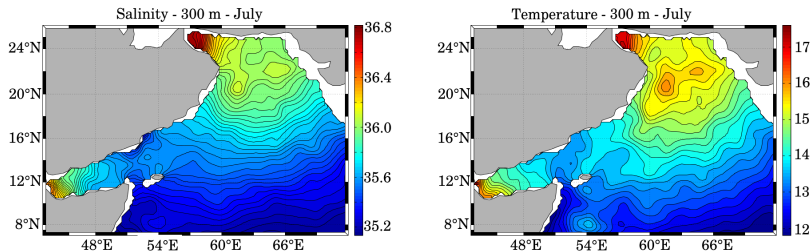
INTRO

CONTEXT - GEOGRAPHY



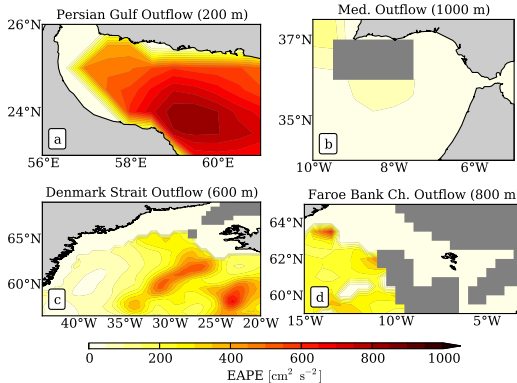
CONTEXT - OUTFLOW PROPERTIES

- Persian Gulf Outflow (warm and salty waters) through the Strait of Hormuz (~ 40 - 100 m).
- Neutral buoyancy at ~ 200 - 300 m.



[climatologies derived from ARGO floats (2006-2010), figures from Carton et al. 2012]

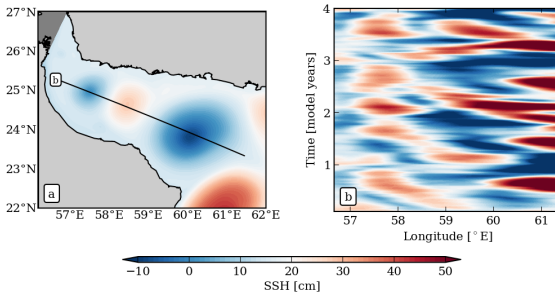
CONTEXT - DYNAMICAL ENVIRONMENT



[Eddy Available Potential Energy derived from ARGO floats, Roulet et al. 2014]

- Shallow equilibrium depth ($\sim 200\text{-}300$ m)
- Western Boundary : high level of mesoscale turbulence (remotely forced)

CONTEXT - DYNAMICAL ENVIRONMENT



- Shallow equilibrium depth ($\sim 200\text{-}300\text{ m}$)
- Western Boundary : high level of mesoscale turbulence (remotely forced)
- Confined environment : westward drifting eddies are trapped and interact with the topography (continental slope)

Similarity with the Red Sea Outflow → Eddy-outflow interactions are to be expected [Illicak et al. 2011, Bower & Furey 2012]

ISSUES & METHODS

Issues

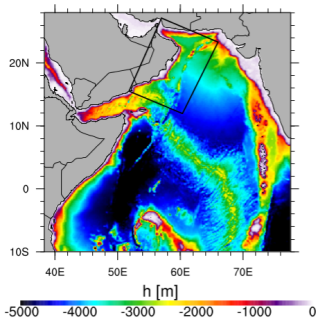
How mesoscale eddies interact with the Persian Gulf Outflow ?
How is Persian Gulf Water (PGW) spread in the Gulf of Oman ?

Methods

- High resolution (2 km) nested regional numerical simulation (ROMS)
- Idealized simulations (ROMS)

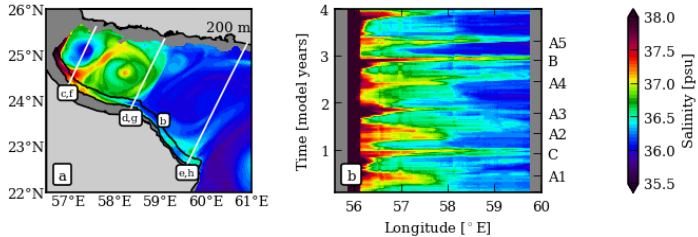
PHENOMENOLOGY

REALISTIC SIMULATION (4 YEARS)



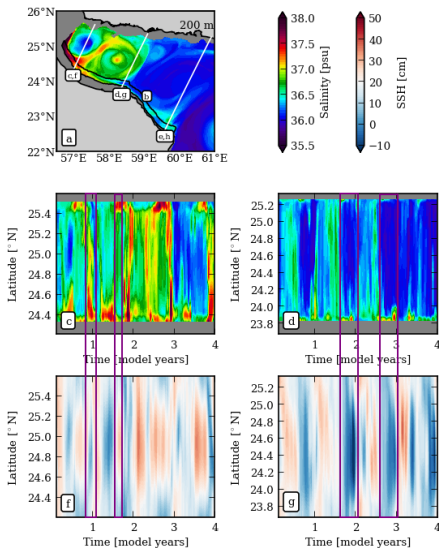
- ROMS one-way nested configuration (black rectangle) from an Arabian Sea solution at $\Delta x = 6.6$ km.
- $\Delta x = 2$ km, submesoscale permitting ($R_d = 41$ km).
- Monthly climatological forcing : QuikSCOW wind stress and ICOADS heating and freshwater fluxes.
- Semi-analytical western boundary in the shallow Strait of Hormuz from moored ADCPs and T-S measurements [Johns et al. 2003]

AN INTERMITTENT SLOPE CURRENT CONTAINING PGW



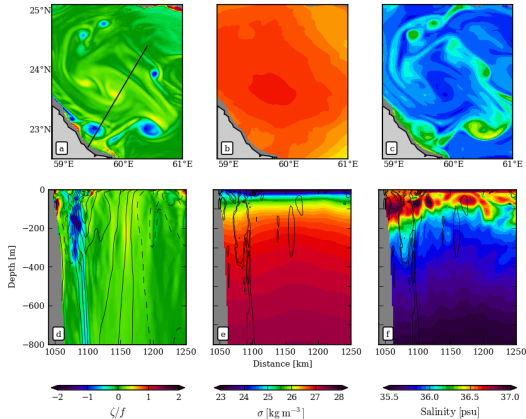
- The slope current is discontinuous and intermittent along the southern boundary (expected from Coriolis force).
- Salt is rapidly diluted from the Strait to the end of the Gulf.

ROLE OF MESOSCALE EDDIES



- The fate of the outflow is tightly linked with surface intensified mesoscale eddies, at a seasonal time scale.
- Cyclones steer PGW southward.
 - Anticyclones steer PGW northward.

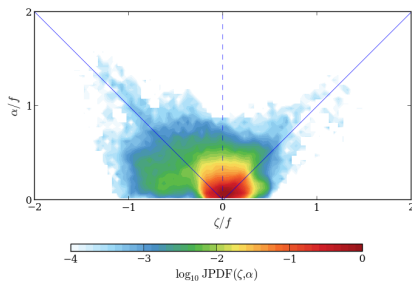
SUBMESOSCALE COHERENT VORTICES (SCVS) CONTAIN PGW



- Mesoscale eddies, remotely formed and propagating into the Gulf, detach fragments of PGW from the slope.
- PGW is trapped into, above or beneath SCVs.

- SCV properties : $|\zeta|/f \sim 1$, $L < R_d$, core located at depth $\sim 100\text{-}300$ m
- polarity : opposed to the neighbouring mesoscale eddy,
- trajectory : advection along the edges of mesoscale eddies.

SCV LIFE CYCLE



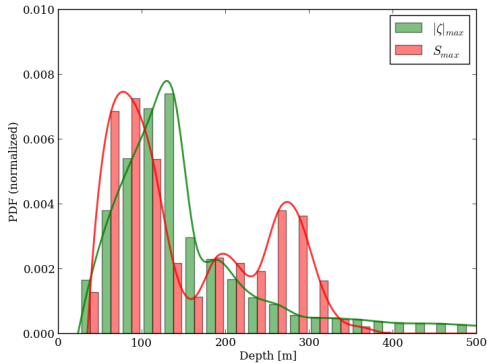
Joint Probability Density Function of

$$\zeta = v_x - u_y \text{ and}$$

$$\alpha = [(v_x + u_y)^2 + (u_x - v_y)^2]^{1/2}.$$

- Short life cycle :
< 10 days
- Strong surrounding deformation field :
 - $\text{div. } \delta = u_x + v_y \sim f$
 - shear $s = v_x + u_y \sim f$
 - strain $\sigma = u_x - v_y \sim f$
 Thus competing with ζ .
- Limit of resolution of the model ?

PASSIVE ROLE OF THE OUTFLOW ?



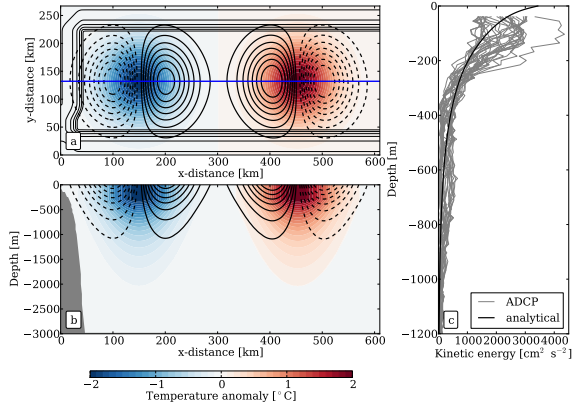
- Non Co-localization of the salt (hydrological) and relative vorticity (dynamical) cores.
- PGW is embedded into SCVs but is not necessarily in their cores.

→ How SCVs are formed ?

→ Is the outflow passive in the formation of SCVs ?

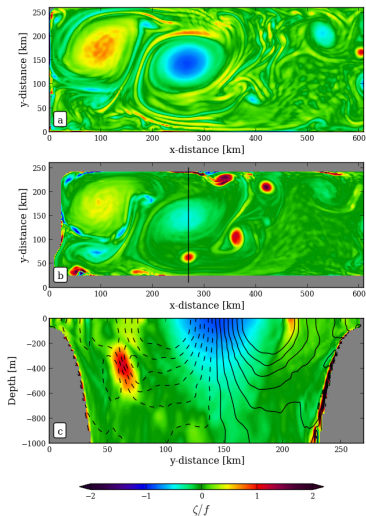
PROCESSES

IDEALIZED EXPERIMENT - SET UP



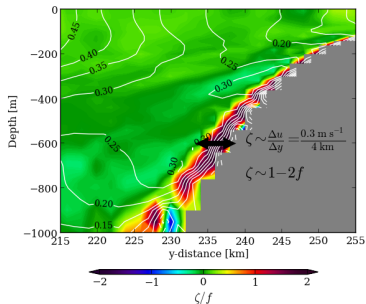
- Idealized Gulf of Oman : extents, R_d , Δx , ...
- Free decay of mesoscale eddies with a realistic energy level.
- With/without bottom friction (linear drag, $C_D = 3 \cdot 10^{-4} \text{ m s}^{-1}$)

BOUNDARY LAYER DYNAMICS



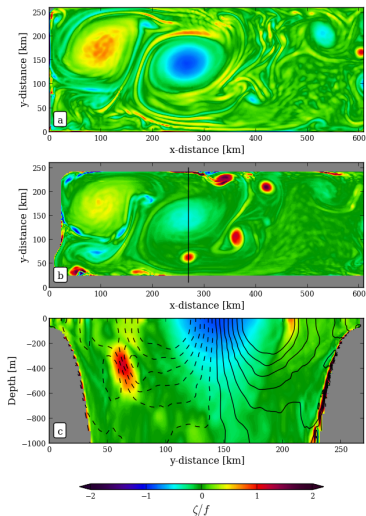
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BOUNDARY LAYER DYNAMICS



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- Intense vorticity strips are generated in boundary layers $|\zeta|/f > 1$. They roll up in the interior into SCVs, being unstable for the centrifugal instability ($\zeta < 0$) or barotropic (shear) instability ($\zeta > 0$) [D'Asaro 1988, Molemaker et al. 2014, Gula et al. 2015].

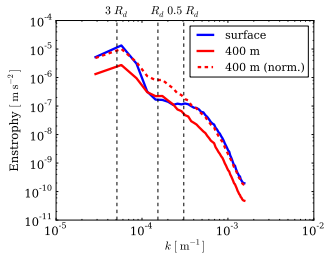
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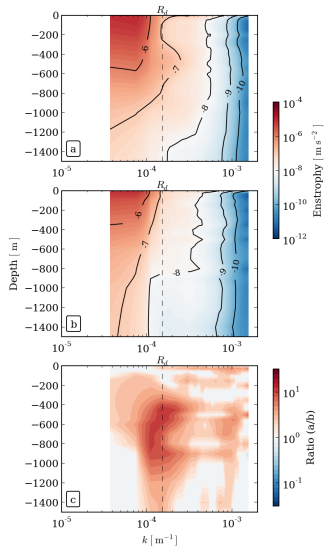
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- Friction acts on mesoscale eddy velocity and neither topographic irregularity nor density current is required for detachment of SCVs.

ENSTROPY SOURCE ON THE CONTINENTAL SLOPE

→ The enstrophy $\zeta^2/2$ source is localized on the continental slope where mesoscale eddies drag.

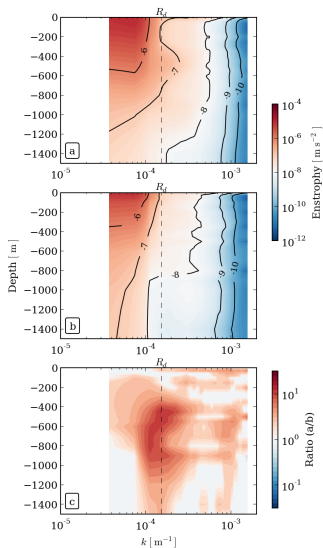


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- Experiments with/without bottom stress highlight that the enstrophy source is due to friction.
- The ROMS model (σ -coordinates) vertical boundary layer implies a horizontal shear layer

[Molemaker et al. 2014, Gula et al. GRL 2015].

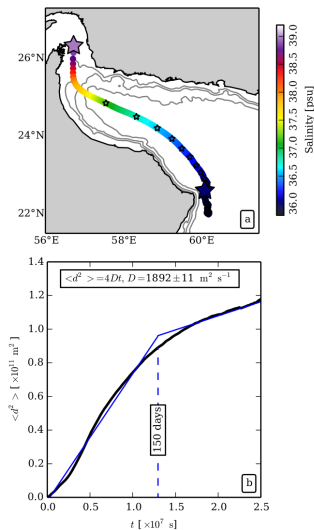
CONSEQUENCES

LAGRANGIAN PERSPECTIVE

- Continuous release of synthetic particles in the Strait at the outflow depth

[code described in Gula et al. JPO 2014]

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- Diffusion-like dispersion of particles : linear in time, typical of a random-walk process.

$$\langle d^2(t) \rangle = 4D t$$

- Eddy diffusivity $D \sim 2000 \text{ m}^2 \text{ s}^{-1}$, similar to highly diffusive regimes (ACC, $D \sim 3000 \text{ m}^2 \text{ s}^{-1}$)

[Abernathey et al. 2010]

CONCLUSIONS

CONCLUSION

How mesoscale eddies interact with the Persian Gulf Outflow ? How is PGW spread in the Gulf of Oman ?

- Eddy-topography interactions produce high vorticity strips that roll up into Submesoscale Coherent Vortices. Friction is responsible for the generation of enstrophy in boundary layers, especially on the continental slope.
- These SCVs trap Persian Gulf Water and participate actively to its spreading in the Gulf of Oman.
- Small-scale eddy-topography interactions lead to turbulent diffusion processes that have a large-scale effect on the salt distribution.

SENSITIVITY TO THE BOTTOM STRESS [1/2]

How is the boundary layer sensitive to the bottom stress parameterization?

Same experiments with :

1. Linear bottom stress : $\boldsymbol{\tau}_b = -\rho_0 C_D^{lin} \mathbf{u}$, constant C_D
2. Quadratic bottom stress : $\boldsymbol{\tau}_b = -\rho_0 C_D^{quad} \|\mathbf{u}\| \mathbf{u}$, constant C_D
3. Quadratic bottom stress with a variable C_D :

$$C_D^{VonKarman} = \left(\frac{\kappa}{\log(\Delta z_b / z_r)} \right)^2,$$

$\kappa = 0.41$: Von Karman constant,

z_r : roughness parameter $O(10^{-2} - 10^{-3} \text{ m})$

SENSITIVITY TO THE BOTTOM STRESS [2/2]

Type	C_D	$\langle \boldsymbol{\tau} \rangle$ [$\times 10^{-3} \text{ N m}^{-2}$]	$\text{std}(u_{\text{bottom}})$ [cm s^{-1}]
Linear	$3.0 \cdot 10^{-4} \text{ m s}^{-1}$	12.4	4.7
Linear	$6.0 \cdot 10^{-4} \text{ m s}^{-1}$	17.1 (+38%)	3.3 (-30%)
Quadratic	$2.5 \cdot 10^{-3}$	8.7	5.1
Quadratic	$5.0 \cdot 10^{-3}$	12.2 (+28%)	4.2 (-18%)
Quadratic with Von Karman C_D	varying	7.9	5.1

